

Process for preparing isocyanatoorganosilanes

The invention relates to a process for preparing isocyanatoorganosilane.

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For some time there has been great interest in an economic method for preparing isocyanatoorganosilanes in high yields and purities. Said compounds are of great economic importance since they are used, for 10 example, industrially as adhesion promoters between organic polymers and inorganic materials (also termed coupling agents, crosslinkers).

For their preparation, processes are preferred in which 15 the starting materials are almost completely safe or completely safe in order to facilitate handling and procedure. In the case of the processes previously used, however, isocyanatoorganosilanes are prepared in relatively low amounts, and in low-efficiency and 20 expensive processes.

For instance, in the process described in US 6,008,396, carbamatoorganosilanes are converted in inert hot media to the isocyanates, with elimination of alcohol. 25 However, this process can only be operated semi-continuously, since the concentration of impurities in the medium, even after a short time, increases in such a manner that the desired purity of the product is no longer ensured.

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In the process described in US 3,598,852, carbamato-organosilanes are vaporized in vacuum and the isocyanatosilane formed is distilled off continuously.

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In the process described in EP 1010704 A2 carbamatoorganosilanes are thermally cleaved in the liquid phase to give the corresponding isocyanatoorganosilanes with catalysis by Sn(II)

chloride. Particularly the highly complex process for isolating and purifying the desired products which leads to low yields has been found disadvantageous in this process, and thus it appears not to be of interest 5 for application on an industrial scale.

EP 649850 B1 discloses the thermal cleavage (thermolysis) of carbamatoorganosilanes in the gas phase at atmospheric or reduced pressure. However, the 10 yields obtainable by this process, in particular of isocyanatomethylorganosilanes, are unsatisfactory under the conditions described there.

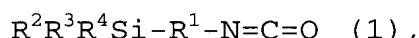
The object was therefore to provide a further process 15 for preparing isocyanatoorganosilanes which solves the problems known from the prior art.

The object is achieved by the thermolysis being induced by exposure to microwave radiation.

20 The invention relates to a process for preparing isocyanatoorganosilanes by thermolysis of carbamato-organosilanes wherein the thermolysis takes place by exposure to microwave radiation.

25 The term "microwaves" is taken to mean here electromagnetic oscillations having a frequency of 300 MHz to 300 GHz.

30 In a preferred embodiment of the inventive process, isocyanatoorganosilanes of the general formula (1) are prepared



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where

R is a monovalent C₁-C₁₀-alkyl radical,

R¹ is a divalent C₁-C₆-hydrocarbon radical and

R², R³ and R⁴ are in each case independently of one another, a methyl, ethyl, n-propyl, isopropyl, methoxy, ethoxy, n-propoxy or isopropoxy radical,

5 by thermolysis of carbamatoorganosilanes of the general formula (2)



10 In terms of the selectivity and reaction rate that can be achieved, the inventive process offers significant advantages over the prior-art processes.

15 In the process, in general C₁-C₁₀-alcohols of the general formula ROH are eliminated from the carbamatoorganosilanes, in particular those of the general formula (2), by thermolysis, in particular methanol, ethanol, propanol, butanol, isobutanol, pentanol, hexanol, isohexanol, cyclohexanol and 20 2-ethylhexanol. Preferably, methanol and ethanol, particularly preferably methanol, are eliminated.

25 By means of the inventive process, it is generally possible to prepare isocyanatoorganosilanes containing short-chain spacers between the Si atom and the isocyanate function, which have been available hitherto only with difficulty and in moderate yields, in particular those isocyanatoorganosilanes of the general formula (1) where **R¹** is methylene.

30 As spacer **R¹** between the organosilyl group and the carbamato group, use can generally be made of linear or branched saturated or unsaturated C₁-C₆-hydrocarbon groups. Preferred spacers **R¹** are alkyl radicals, in 35 particular linear alkyl radicals; particularly preferably, use is made of methylene, ethylene and propylene.

R^2 , R^3 and R^4 are preferably methyl, methoxy, ethoxy, n-propoxy or isopropoxy radicals.

5 By means of the inventive process, in particular compounds of the general formula 1 where

R^2 , R^3 = methoxy, R^4 = methyl and R^1 = methylene; or
 R^2 = methoxy, R^3 = ethoxy, R^4 = methyl and R^1 = methylene; or

10 R^2 , R^3 = ethoxy, R^4 = methoxy and R^1 = methylene; or
 R^2 , R^3 = methoxy, R^4 = ethoxy and R^1 = methylene,

can be prepared in high yields and purities.

15 The inventive process can optionally be carried out in the presence of a catalyst. Catalysts which come equally into consideration are in principle homogeneous and heterogeneous catalysts.

20 Suitable homogeneous catalysts are one or more compounds selected from the group consisting of soluble tin, lead, cadmium, antimony, bismuth, titanium, zirconium, niobium, iron, cobalt, manganese, chromium, molybdenum, tungsten, nickel, copper and zinc
25 compounds, and also soluble organic nitrogen bases.

In particular, suitable compounds are 1,4-diazabicyclo-[2.2.2]octane, dibutyltin dilaurate, dibutyltin maleate, dibutyltin diacetate and dimethyltin
30 dichloride.

As heterogeneous catalysts, use can be made in general of metals and/or compounds comprising elements selected from the group Sn(I), Sn(II), Pb(II), Zn(II), Cu(I),
35 Cu(II), Co(I), Co(II), Na, K, Li, Rb, Cs, Sr, Ba, Mg, Ca, Cr, Mo, Ti, V, W, Ce, Fe, Ni, Si, Al, Ge, Ga, In, Sc, Y, La, lanthanides, Pd, Pt, Co, Rh, Cu, Ag, Au, Zn, Cd, N, B, C, and their mixtures and alloys comprising

the abovementioned elements.

Preferred heterogeneous catalysts are oxides, hydroxides, oxyhydroxides, mixed oxides, acetates, 5 formates, oxalates, tartrates, citrates, nitrates, carbonates, or mixtures of the abovementioned compounds of one or more elements selected from the group consisting of Sn(I), Sn(II), Pb(II), Zn(II), Cu(I), Cu(II), Co(I), Co(II), Na, K, Li, Rb, Cs, Sr, Ba, Mg, 10 Ca, Cr, Mo, Ti, V, W, Ce, Fe, Ni, Si, Al, Ge, Ga, In, Sc, Y, La, lanthanides, Pd, Pt, Rh, Cu, Ag, Au and Cd.

In particular, suitable heterogeneous catalysts are those comprising one or more compounds selected from 15 the group consisting of TiO_2 , ZrO_2 , HfO_2 , Al_2O_3 , BaO , CaO , MgO , CeO_2 , La_2O_3 , Y_2O_3 , Sm_2O_3 , Yb_2O_3 , Cr_2O_3 , ZnO , V_2O_4 , MnO_2 , NiO , In_2O_3 , Ga_2O_3 , GeO_2 , FeO , Fe_2O_3 , Fe_3O_4 , 20 CuO , Co_3O_4 , $Fe(MoO_4)_3$, $MgO/CsOH$, $MgO/NaOH$, alumino-silicates, in particular zeolites in different pore sizes, cordierite of the composition $2\ MgO \cdot 2\ Al_2O_3 \cdot 5\ SiO_2$, heteropolyacids, carbon modifications, e.g. graphite, transition metal nitrides, transition metal borides, transition metal silicides and carbides.

25 These metals, metal compounds or their mixtures can also be applied to porous or non-porous support materials. Particularly suitable supports made of inert refractory materials are oxidic and nonoxidic ceramic, SiO_2 , carbon, aluminosilicates, magnesium alumino-silicates or resistant metallic materials, in 30 particular glass wool, quartz wool, ceramics, oxidic compositions, such as SiO_2 , Al_2O_3 , Fe_2O_3 or steatite.

35 The catalyst supports can be used in the form of irregular granules, spheres, rings, half-rings, saddles, cylinders, trilobes or monoliths.

The inventive process is generally carried out with

microwaves in the frequency range from 300 MHz to 300 GHz, particularly in the ISM frequency bands with the central frequencies of 896 MHz, 915 MHz, 922 MHz, 2.45 GHz, 5.8 GHz, 24.1 GHz, 61 GHz, 122 GHz, 245 GHz, 5 more preferably at 915 MHz, 2.45 GHz and 5.8 GHz. The 10 microwaves are generated using generators having known active components such as electron tubes such as, for example, magnetron, klystron, gyrotron or semiconductor amplifiers. Preference is given to air-cooled or water-cooled 15 magnetrons having individual transmission outputs of 100 W to 100 kW, more preferably 300 W to 30 kW. The reaction, initiated by the irradiation of the reactants with microwaves, must be carried out in a reaction chamber which is suitable for irradiation with 20 microwaves. Suitable materials for the reaction chamber are chemically stable materials permeable to microwaves, such as, for example, microwave-transparent glasses, quartz glass, microwave-transparent oxidic ceramics, microwave-transparent nonoxidic ceramics, or 25 chemically stable materials which are impervious to microwaves, such as, for example, metals which, for the irradiation of the microwaves, are equipped with windows made from microwave-transparent material such as, for example, microwave-transparent glasses, quartz glass, microwave-transparent oxidic ceramics, or 30 microwave-transparent nonoxidic ceramics. The microwaves are coupled radiatively into the reaction chamber via known components such as launchers, hollow wave guides, tuners, circulators, insulators, slot antennas, irises or direct generators.

The reaction chamber can be free or provided with 35 internals. The internals affect the flow distribution, temperature distribution and microwave distribution in the reaction chamber. The internals can consist of microwave-transparent material such as microwave-transparent glasses, quartz glass, microwave-transparent oxidic ceramic, microwave-transparent non-

oxidic ceramic and then affect only the fluid flow in the reaction space. If the internals consist of microwave-reflecting material (e.g. high-conductivity metals, graphite) or microwave-absorbent materials 5 (especially ceramics, silicon carbide, magnetic materials or electric resistance materials), the microwave distribution and temperature distribution are also affected.

10 In the reaction chamber, when the inventive process is optionally carried out in the presence of a catalyst, one or more of the abovementioned heterogeneous catalysts can be present or introduced continuously, together with the internals or alone.

15 The reaction chamber can also be constructed in such a manner that the entire reaction space or a part of the reaction space is filled with a fluidized solid, the solid being able to act as microwave absorber, heat 20 carrier and/or catalyst.

For the general design of microwave irradiation systems, reference may also be made at this point to literature such as A. Mühlbauer, "Industrielle Elektro-25 wärmetechnik" [Industrial Electrical Heating Technology], Essen Vulkan-Verlag, 1992; D.M.P. Mingos, "The Application of Microwaves to the Processing of Inorganic Materials", British Ceramic Transactions, 91, 1992; G. Orth, "Mikrowellenerwärmung in der Industrie" 30 [Microwave Heating in Industry] RWE-Industrieforum, Essen, 1993.

The process can generally be carried out batchwise, semicontinuously, or continuously. Preference is given 35 to continuously distilling off one or more volatile reaction products from the reaction chamber, both the reaction product alcohol and the reaction product iso-cyanoatoorganosilane being able to be distilled off

separately or together.

In one preferred embodiment of the inventive process the reaction chamber is introduced into a distillation column, forming a reactive distillation. The high-boiling reaction products can be taken off in the liquid phase of the column, below the reaction chamber, while the volatiles can be taken off at the top of the column, above the reaction chamber. Middle fractions may be drawn off not only between the reaction section and the top of the column but also between the reaction section and the liquid phase of the column.

The carbamatoorganosilanes, especially those of the general formula (2), are reacted preferably in a temperature range of 150-500°C, particularly preferably in a range of 200-400°C, in particular in a range of 250-350°C, under microwave irradiation. The temperature here may be attained by microwave irradiation alone or by a combination of conventional heating and microwave radiation. The conventional heating power may be introduced at the same time as or sequentially to the microwave irradiation. A further possibility is to combine the microwave heating with conventional cooling so as to allow a higher microwave radiation intensity to be applied while observing a specified temperature.

The microwave power is selected such that, under the other boundary conditions of the heat balance in the reaction zone, such as heat supply and heat removal via insulation losses, conventional cooling or heating, heat supply and heat removal via the latent heat of the reaction mixture, evaporative cooling of the reaction mixture, cooling or heating by injection of cold and/or hot inert gases and/or liquids or reactants, it is possible to maintain a preselected reaction temperature.

The process can be carried out with or without a carrier gas, e.g., nitrogen, hydrogen, air, noble gases, such as helium or argon, vapors of carbon-containing substances such as carbon monoxide, carbon 5 dioxide, methane, octane, toluene, decalin or tetralin; the carrier component may also be added in liquid form and then not evaporated until it is in the heated zone, forming a gas stream.

10 By means of the carrier gas, it is possible to dilute, heat or cool the reaction mixture, fluidize and/or transport solids and set defined flow conditions.

15 The inventive process is preferably carried out in a pressure range of 0.01 -100 bar, particularly preferably at 0.5 -40 bar, in particular in a range of 1-10 bar.

20 The inventive process, compared with the processes known from the prior art, has the great advantage that the desired products can be obtained in a simple downstream distillation step in high purity (>97%). The formation of six-membered isocyanurates observed at high thermal stresses is virtually completely avoided 25 by the present process.

In one specific embodiment of the inventive process the reaction chamber in which microwave irradiation occurs (microwave reaction chamber) is followed by a reaction 30 zone (afterreaction zone) optionally containing a heterogeneous catalyst.

Since, owing to density, gases absorb microwave radiation only to a very small extent, the process can be provided advantageously with an afterreaction zone 35 in which the mixture partly or fully vaporized in the microwave irradiation zone and containing carbamateorganosilane vapor is reacted further to isocyanate organosilanes. Particularly preferred

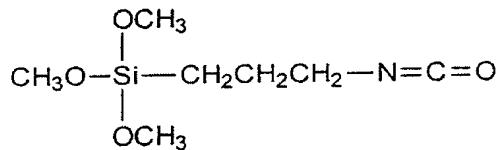
embodiments of the afterreaction zone are gas-phase reactors filled with a heterogeneous catalyst, the heterogeneous catalysts being selected from the abovementioned embodiments optionally applied to the 5 abovementioned support materials.

The examples which follow serve to illustrate the inventive process and are in no way to be viewed as a restriction.

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Comparative example:

Preparation of γ -isocyanatopropyltrimethoxysilane from methylcarbamatopropyltrimethoxysilane



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20 ml of methylcarbamatopropyltrimethoxysilane together with 2 g of Fe_2O_3 catalyst were heated very rapidly to 225°C, using an oil bath, in a glass reaction vessel with distillation still and overhead condenser. Within 20 a reaction time of 60 minutes no overhead condensate was formed. GC analysis of the contents of the still revealed the following composition:

96% by weight methylcarbamatopropyltrimethoxysilane

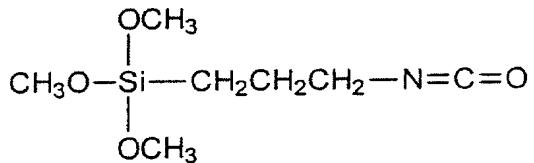
0.9% by weight γ -isocyanatopropyltrimethoxysilane

25 0.5% by weight methanol

2.6% by weight by-products

Example 1:

Preparation of γ -isocyanatopropyltrimethoxysilane from methylcarbamatopropyltrimethoxysilane with microwave irradiation



20 ml of methylcarbamatopropyltrimethoxysilane were irradiated with a microwave power of 300 W (frequency 5 2.45 GHz) in a microwave oven in a glass reaction vessel with distillation still and overhead condenser. Within a reaction time of 5 minutes the overhead temperature rose to 218°C. At this temperature the experiment was ended. 0.7 ml of overhead condensate was 10 formed. GC analysis of the contents of the still revealed the following composition:

90% by weight methylcarbamatopropyltrimethoxysilane
6.1% by weight γ -isocyanatopropyltrimethoxysilane
3.9% by weight by-products

15 GC analysis of the overhead condensate revealed the following composition:

10% by weight methylcarbamatopropyltrimethoxysilane
3% by weight γ -isocyanatopropyltrimethoxysilane
85% by weight methanol

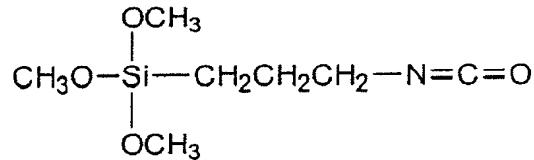
20 Whereas in the comparative example only 0.8 ml of methylcarbamatopropyltrimethoxysilane was converted in 60 minutes, in the inventive example 2.6 ml of methylcarbamatopropyltrimethoxysilane are converted in 5 minutes (40-fold reaction rate).

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Example 2:

Preparation of γ -isocyanatopropyltrimethoxysilane from methylcarbamatopropyltrimethoxysilane with microwave irradiation

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20 ml of methylcarbamatopropyltrimethoxysilane together with 2 g of Fe_2O_3 catalyst were irradiated with a microwave power of 300 W (frequency 2.45 GHz) in a 5 microwave oven in a glass reaction vessel with distillation still and overhead condenser. Within a reaction time of 4 minutes the overhead temperature rose to 165°C. At this temperature the experiment was ended. 1.7 ml of overhead condensate was formed. GC 10 analysis of the contents of the still revealed the following composition:

85% by weight methylcarbamatopropyltrimethoxysilane

12.5% by weight γ -isocyanatopropyltrimethoxysilane

2.5% by weight by-products

15 GC analysis of the overhead condensate revealed the following composition:

25% by weight methylcarbamatopropyltrimethoxysilane

16% by weight γ -isocyanatopropyltrimethoxysilane

55% by weight methanol

20 Whereas in the comparative example only 0.8 ml of methylcarbamatopropyltrimethoxysilane was converted in 60 minutes, in the inventive example 4 ml of methylcarbamatopropyltrimethoxysilane are converted in 4 minutes (75-fold reaction rate). While in the 25 comparative example by-products are formed in an amount of almost 300% of the target product, the inventive process only gives a by-product fraction of less than 20%.